

# Active Filter Circuits

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## Active Filter Circuits

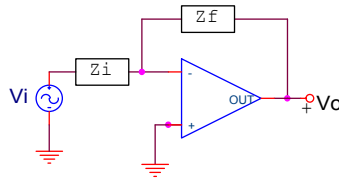
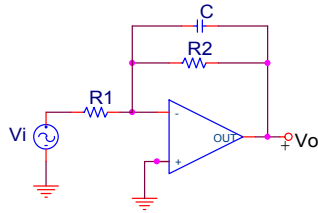
### Introduction

Filter circuits with RLC are passive filter circuit  
Use op amp to have active filter circuit  
Active filter can produce band-pass and band-reject filter without using inductor.  
Passive filter incapable of amplification. Max gain is 1  
Active filter capable of amplification  
The cutoff frequency and band-pass magnitude of passive filter can change with additional load resistance  
This is not a case for active filters

We look at few active filter with op amps.  
We look at that basic op amp filter circuits can be combined to active specific frequency response and to attain close to ideal filter response

## Active Filter Circuits

### First-Order Low-pass Filters



Transfer function of the circuit

$$H(s) = \frac{-Z_f}{Z_i}$$

$$H(s) = \frac{-R_2 \parallel \frac{1}{sC}}{R_1} = \frac{-R_2}{R_1} \frac{1}{sR_2C + 1}$$

$$H(s) = \frac{-R_2}{R_1(sR_2C + 1)}$$

$$H(s) = -K \frac{\omega_c}{(s + \omega_c)}$$

The Gain

$$K = \frac{R_2}{R_1}$$

Cutoff frequency

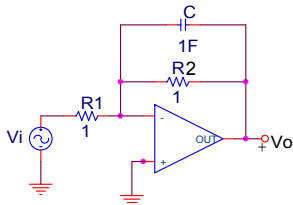
$$\omega_c = \frac{1}{R_2C}$$

Transfer function in  $j\omega$

$$H(j\omega) = -K \frac{1}{(1 + j\frac{\omega}{\omega_c})}$$

## Active Filter Circuits

### Example



- Find  $R_2$  and  $C$  values in the following active Low-pass filter for gain of 1 and cutoff frequency of 1 rad/s.

From the gain

$$K = \frac{R_2}{R_1} = 1$$

$$R_2 = R_1 = 1\Omega$$

From the cutoff frequency

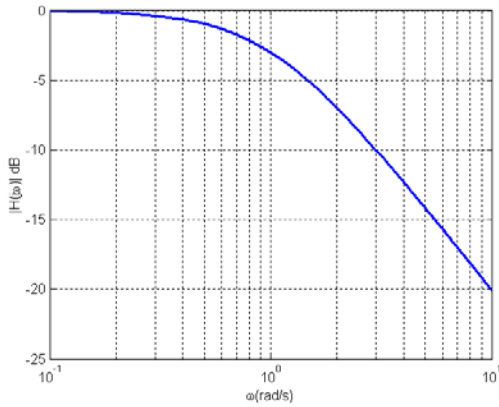
$$\omega_c = \frac{1}{R_2C} = 1$$

$$C = \frac{1}{R_2} = 1F$$

$$H(j\omega) = \frac{1}{(1 + j\frac{\omega}{1})}$$

## Active Filter Circuits

### Example



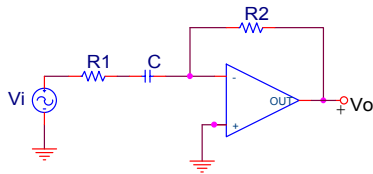
```

>> w=0.1:1:10;
>> h=20*log10(abs(1./(1+j*w)))
;
>> semilogx(w,h)
>> grid on
>> xlabel('\omega (rad/s)')
>> ylabel('|H(j\omega)| dB')
>>
    
```

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## Active Filter Circuits

### A first order high-pass filter



Transfer function of the circuit

$$H(s) = \frac{-Z_f}{Z_i}$$

$$H(s) = \frac{-R_2}{R_1 + \frac{1}{sC}} = \frac{-R_2 s C}{R_1 s C + 1}$$

$$H(s) = \frac{-R_2 s}{R_1(s + \frac{1}{R_1 C})}$$

$$H(s) = -K \frac{s}{(s + \omega_c)}$$

The Gain

$$K = \frac{R_2}{R_1}$$

Cutoff frequency

$$\omega_c = \frac{1}{R_1 C}$$

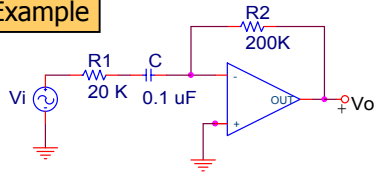
Transfer function in  $j\omega$

$$H(j\omega) = -K \frac{j\omega}{(1 + j\frac{\omega}{\omega_c})}$$

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## Active Filter Circuits

### Example



- Find  $R_2$  and  $R_1$  values in the above active High-pass filter for gain of 10 and cutoff frequency of 500 rad/s.

From the cutoff frequency

$$\omega_c = \frac{1}{R_1 C} = 500$$

$$R_1 = \frac{1}{500C} = 20 \text{ K}\Omega$$

From the gain

$$K = \frac{R_2}{R_1} = 10$$

$$R_2 = R_1 \cdot 10 = 200 \text{ K}\Omega$$

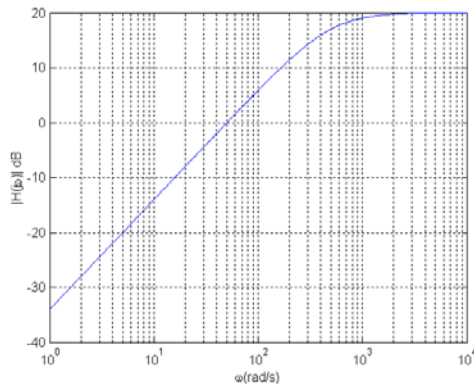
Transfer function in  $j\omega$

$$H(j\omega) = -10 \frac{j\omega}{500} \frac{1}{\left(1 + j\frac{\omega}{500}\right)}$$

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## Active Filter Circuits

### Example



```

>> w=1:10000;
>>
h=20*log10(10*(abs((j*w/500)
)./(1+j*w/500))));
>> semilogx(w,h)
>> grid on
>> xlabel('\omega (rad/s)')
>> ylabel('|H(j\omega)|
dB')
>>
    
```

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## Active Filter Circuits

### Scaling

- In filter design, we can transform RLC values in to realistic values, this process is called **scaling**
- Two types of scaling, **magnitude** and **frequency** scaling
- In **magnitude scaling**, we multiply all L and R by scaling factor  $k_m$ , multiplying all C by  $1/k_m$

$$R' = k_m R$$

$$L' = k_m L$$

$$C' = \frac{C}{k_m}$$

- $k_m$  is positive real number

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## Active Filter Circuits

### Scaling

- **frequency scaling**, we multiply all L, C by  $1/k_f$  where  $k_f$  is scaling factor.

$$R' = R$$

$$L' = \frac{L}{k_f}$$

$$C' = \frac{C}{k_f}$$

- A circuit can be scaled in both magnitude and frequency in simultaneously

$$R' = k_m R$$

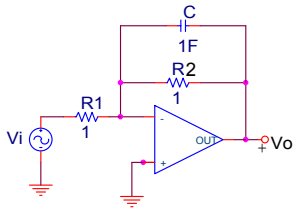
$$L' = \frac{k_m L}{k_f}$$

$$C' = \frac{C}{k_m k_f}$$

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## Active Filter Circuits

### Example



- Example 1 , Find  $R_2$  and  $R_1$  values in the active Low-pass filter for gain of 5 and cutoff frequency of 1Khz and  $c=0.01 \mu\text{F}$

$$k_f = \frac{\omega_c'}{\omega_c} = \frac{2\pi 1000}{1} = 6283.185$$

$$k_m = \frac{1}{k_f} \frac{C}{C'} = \frac{1}{6283.185(10^{-8})} = 15915.5$$

$$R_2' = k_m R_2 = 15915.5(1) = 15.9 \text{ K}\Omega$$

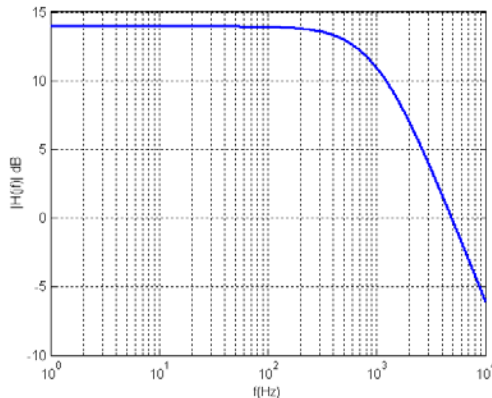
- For gain specification, we need to change  $R_1$

$$R_1 = \frac{R_2}{K} = \frac{15.9\text{K}}{5} = 3.18 \text{ K}\Omega$$

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## Active Filter Circuits

### Example



```
>> f=1:10000;
>> w=2*pi*f;
>>
>> h=20*log10(5*abs(1./(1
+j*w/(2*pi*1000))));
>> semilogx(f,h)
>> grid on
>> xlabel('f (Hz)')
>> ylabel('|H(jf)|
dB')
```

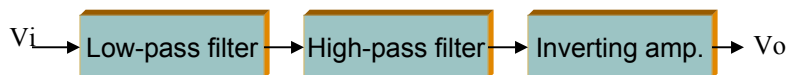
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## Active Filter Circuits

### Op Amp Band-Pass Filters

- Three components
- A unity gain low-pass filter, cutoff frequency is  $\omega_{c2}$
- A unity gain high-pass filter, cutoff frequency  $\omega_{c1}$
- A gain component to provide the desired level

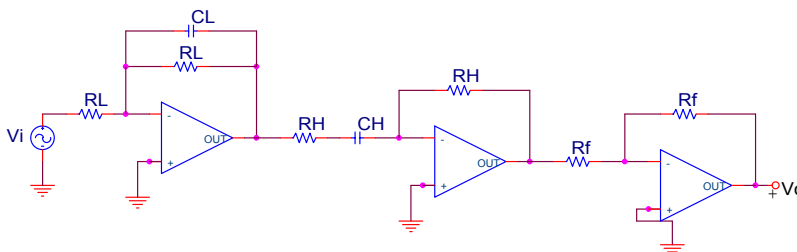
$$\frac{\omega_{c2}}{\omega_{c1}} \geq 2$$



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## Active Filter Circuits

### Op Amp Band-Pass Filters



$$H(s) = \left( \frac{-\omega_{c2}}{s + \omega_{c2}} \right) \left( \frac{-s}{s + \omega_{c1}} \right) \left( -\frac{R_f}{R_i} \right)$$

$$H(s) = \frac{-K\omega_{c2}s}{(s + \omega_{c2})(s + \omega_{c1})}$$

$$H(s) = \frac{-K\omega_{c2}s}{s^2 + (\omega_{c1} + \omega_{c2})s + \omega_{c1}\omega_{c2}}$$

$$H(s) = \frac{\beta s}{s^2 + \beta s + \omega_0^2}$$

$$\omega_{c2} \gg \omega_{c1}$$

$$\omega_{c2} = \frac{1}{R_L C_L}$$

$$\omega_{c1} = \frac{1}{R_H C_H}$$

$$H(j\omega_0) \Big|_{\max} = -K = -\frac{R_f}{R_i}$$

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## Active Filter Circuits

### Example:

- Design a band-pass filter for a graphical equalizer that has gain 2 within the frequency between 100 and 10,000 Hz. Use 0.1  $\mu\text{F}$  capacitors

- For upper cutoff frequency from LP filter

$$\omega_{c2} = \frac{1}{R_L C_L}$$

$$R_L = \frac{1}{\omega_{c2} C_L} = \frac{1}{2\pi 10000(0.1)10^{-6}} = 80 \Omega$$

- For Lower cutoff frequency from HP filter

$$\omega_{c1} = \frac{1}{R_H C_H}$$

$$R_H = \frac{1}{\omega_{c1} C_L} = \frac{1}{2\pi 100(0.1)10^{-6}} = 7958 \Omega$$

- For gain, choose  $R_f = 1\text{K}\Omega$

$$K = \frac{R_f}{R_i}$$

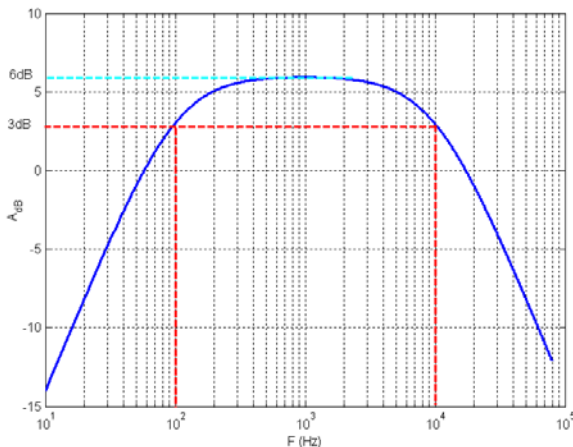
$$R_f = R_i K = 1000(2) = 2 \text{ K}\Omega$$

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## Active Filter Circuits

### From transfer function

$$H(j\omega) = \left( \frac{-2\pi 1000}{j\omega + 2\pi 1000} \right) \left( \frac{-j\omega}{j\omega + 2\pi 100} \right) \left( -\frac{2000}{1000} \right) \quad A_{dB} = 20 \log_{10} |H(j\omega)|$$



```

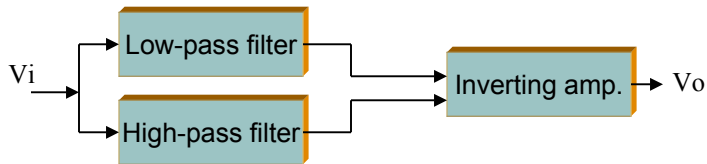
>> f=10:80000;
>> w=2*pi*f;
>> H=(-2*pi*10000)/(j*w+2*pi*10000).*(-j*w)/(j*w+2*pi*100)*(-2);
>> A=20*log10(abs(H));
>> semilogx(f,A)
>> grid on;
>> ylabel ('A_{dB}')
>> xlabel ('F (Hz)')
```

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## Active Filter Circuits

### Op Amp Band-Reject Filters

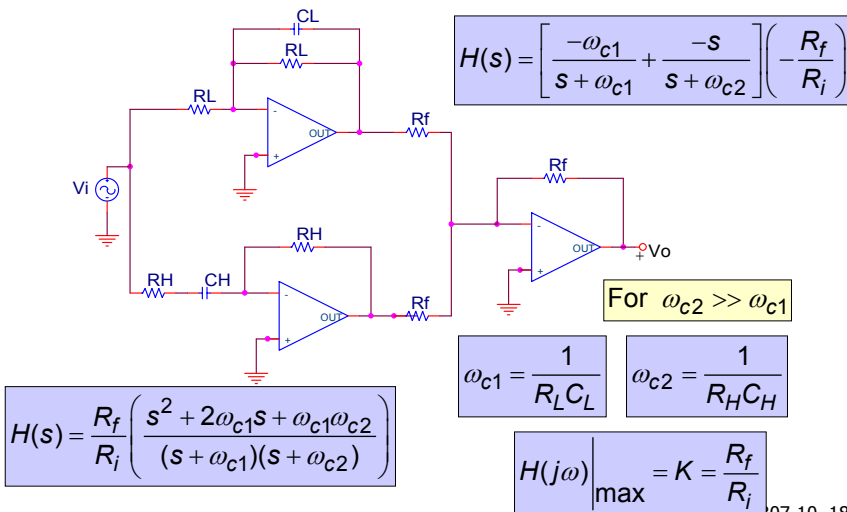
- Three components
- A unity gain low-pass filter, cutoff frequency is  $\omega_{c1}$
- A unity gain high-pass filter, cutoff frequency  $\omega_{c2}$
- A gain component to provide the desired level



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## Active Filter Circuits

### Op Amp Band-Reject Filters



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## Active Filter Circuits

### Example:

- Design an active band-reject filter that has gain 5 and the stop frequency between 100 and 2000 Hz. Use 0.5  $\mu\text{F}$  capacitors

$$F_{c1} = 100\text{Hz and } F_{c2} = 2000\text{Hz} \quad \text{For } \omega_{c2} \gg \omega_{c1}$$

$$\omega_{c1} = \frac{1}{R_L C_L}$$

$$R_L = \frac{1}{\omega_{c1} C_L} = \frac{1}{2\pi 100 (0.5) 10^{-6}} = 3.18 \text{ K}\Omega$$

$$\omega_{c2} = \frac{1}{R_H C_H}$$

$$R_H = \frac{1}{\omega_{c2} C_H} = \frac{1}{2\pi 2000 (0.5) 10^{-6}} = 159 \text{ }\Omega$$

- For gain, choose  $R_f = 1\text{K}\Omega$

$$K = \frac{R_f}{R_i}$$

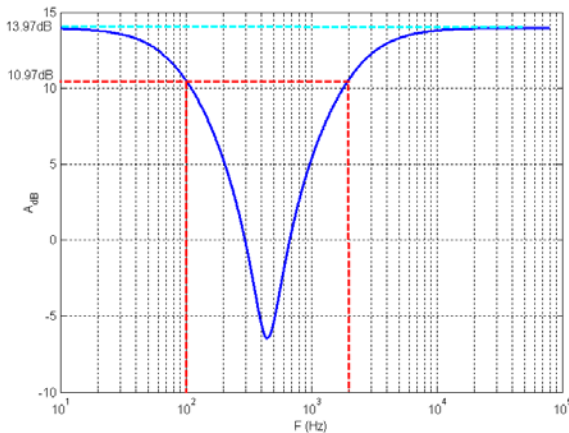
$$R_f = R_i K = 1000(5) = 5 \text{ K}\Omega$$

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## Active Filter Circuits

$$H(j\omega) = \left[ \frac{-\omega_{c1}}{j\omega + \omega_{c1}} + \frac{-j\omega}{j\omega + \omega_{c2}} \right] \left( -\frac{R_f}{R_i} \right)$$

$$A_{dB} = 20 \log_{10} |H(j\omega)|$$



```

>> f=10:80000;
>> w=2*pi*f;
>> H=(((-
2*pi*100)./(j*w+2*pi*100))
+((-
j*w)./(j*w+2*pi*2000)))*(-
5);
>> A=20*log10(abs(H));
>> semilogx(f,A)
>> grid on;
>> xlabel ('F (Hz)')
>> ylabel ('A_{dB}')
```

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